Evidence in focus

Introducing a new modular dual mobility acetabular component: OR30^{\$}

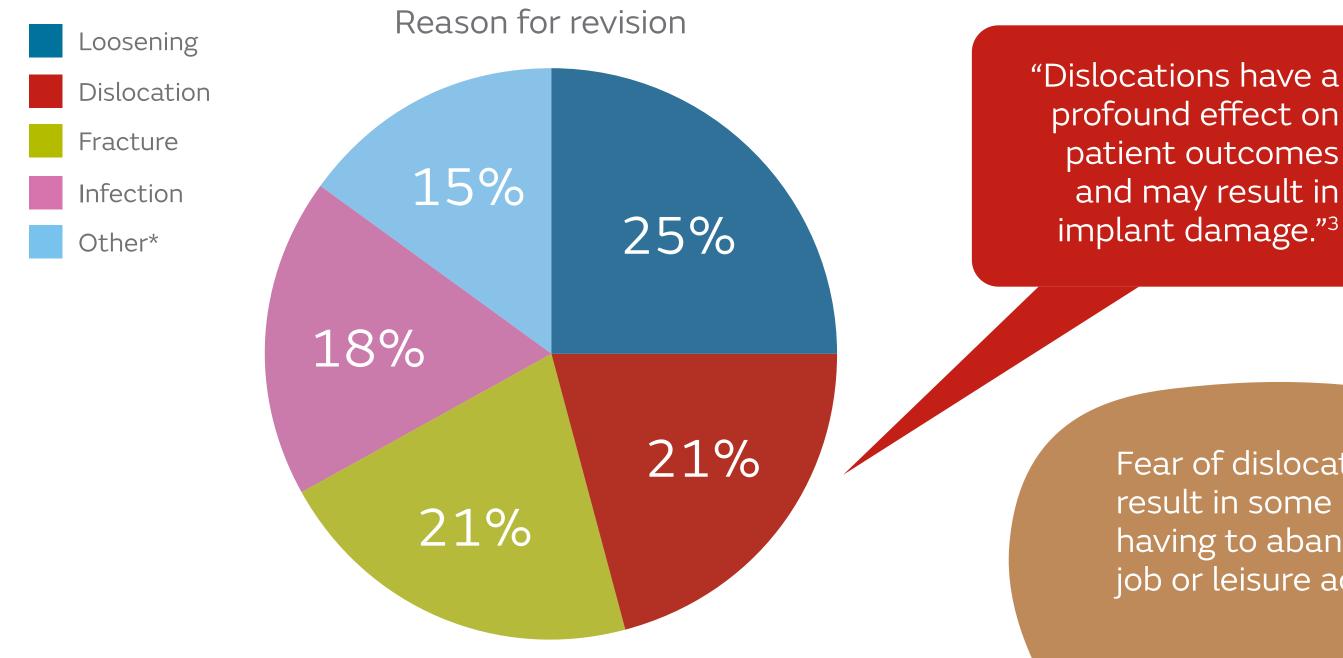
Smith
 Nephew



"Despite the success of primary THR, failure and revision continue to pose a major challenge for orthopaedists while persisting as a significant economic burden on the healthcare system."¹



Dislocation is a leading cause of hip revision²



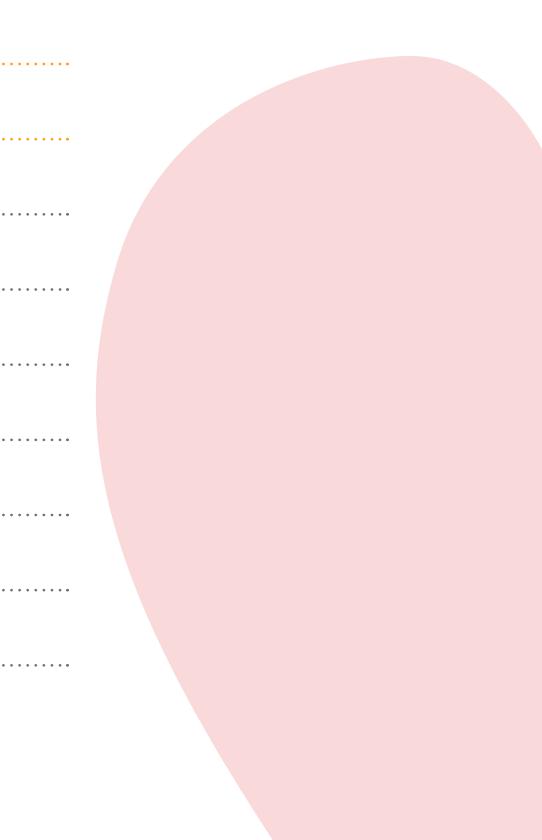
*Includes lysis, pain, leg length discrepancy, malposition, instability, implant breakage. All less than 2.5%.

profound effect on patient outcomes and may result in implant damage."³

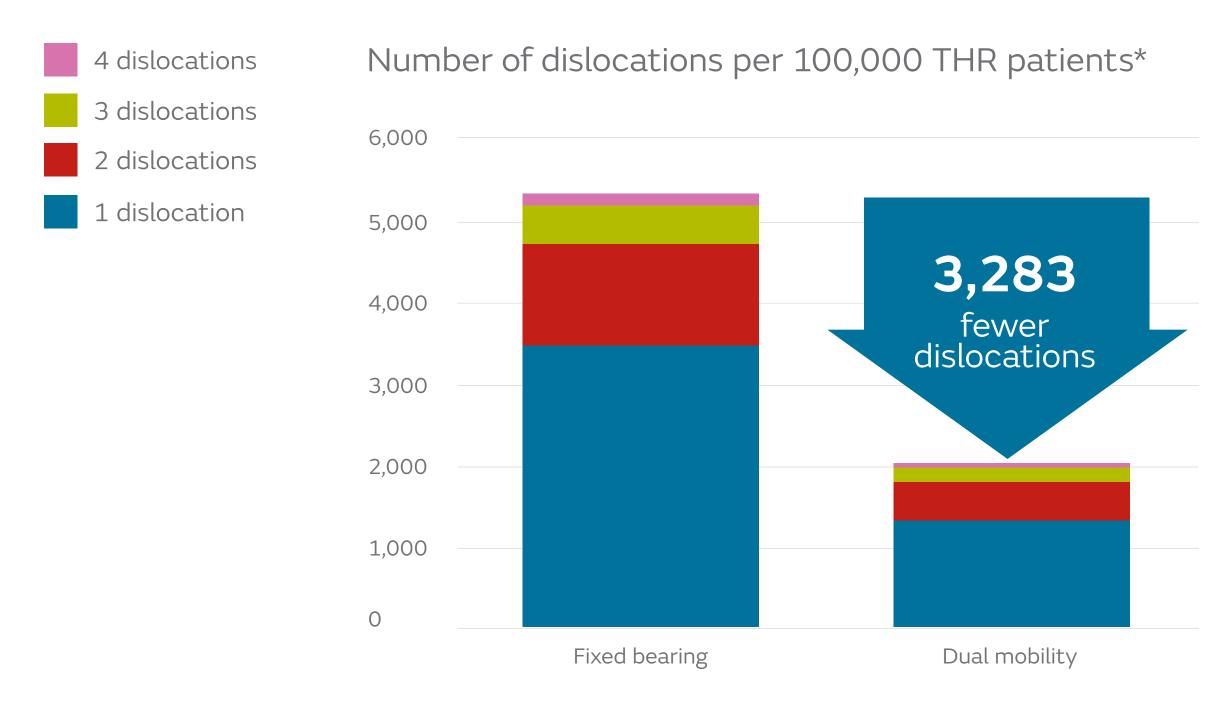
> Fear of dislocation may result in some patients having to abandon their job or leisure activities.⁴

Patient-related risk factors for dislocation⁴⁻⁶

Patient-related risk factors	Preoperative diagnosis
Age >75 years	Avascular necrosis
Female gender aged >70 years	Fractured neck of femur
Prior hip surgery	Inflammatory arthropathy
ASA grade* >3	Neuromuscular disease
Body mass index >30 kg/m²	
Abductor deficiency	
Significant pelvic tilt	
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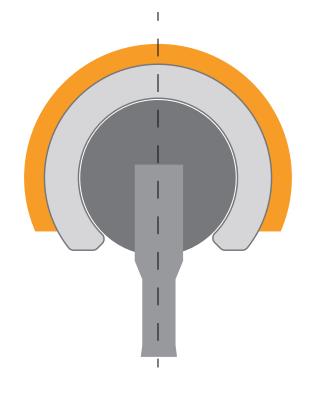
Dual mobility acetabular components may reduce number of dislocations and revisions compared to fixed bearings⁷

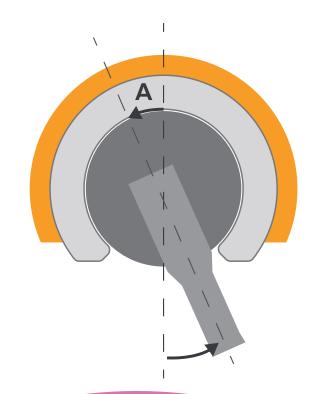


*Based on assuming a relative risk of dislocation of 0.4 for dual mobility vs fixed bearing

Dual mobility (DM) acetabular components

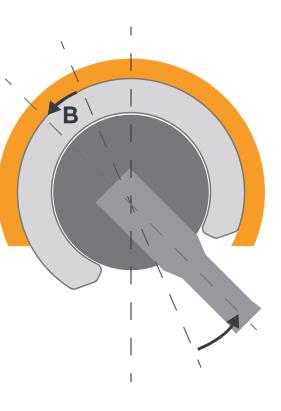
Designed to deliver increased range of motion with good stability to address dislocation whilst reducing wear⁸





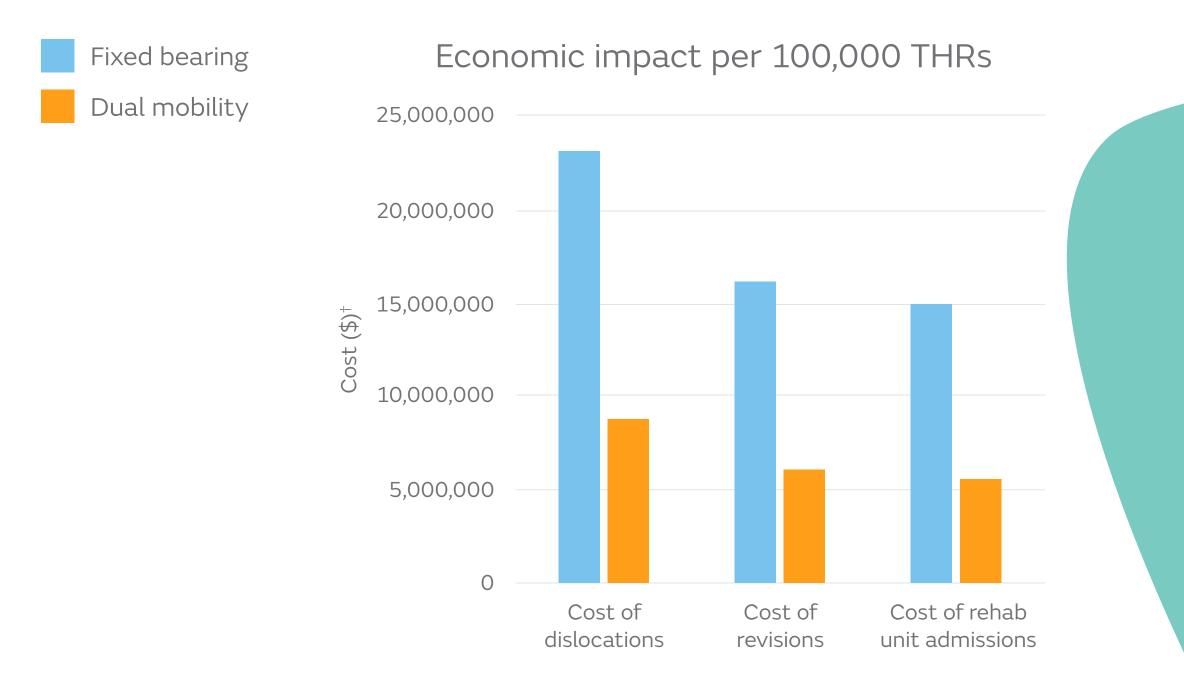
Neutral position The insert is selfaligning, allowing loading following the path of least resistance

Low level activity Primary movement occurs in the ball head/ insert articulation, allowing the insert to sit in its natural position



High level activity Secondary movement occurs in the insert/cup articulation

Potential cost savings with DM cups when used in all primary THR patients*⁷

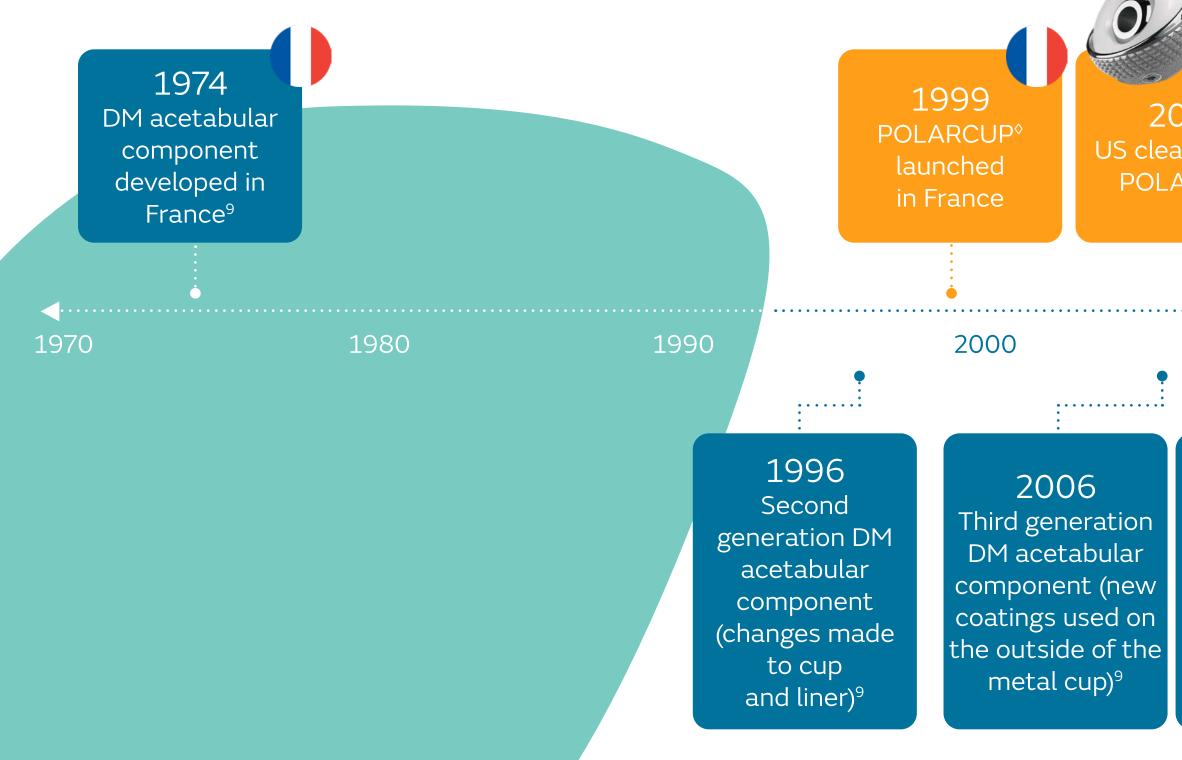


DM cups may result in cost savings per 100,000 primary THRs of \$33,399,671⁺ Dual mobility cups – building on our strong heritage





Advances in dual mobility systems



2007 US clearance of POLARCUP

2017 US clearance of BIRMINGHAM HIP[◊] dual mobility insert

2010

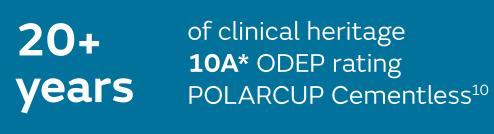
2020

2010 US clearance of modular dual mobility acetabular components

(MDM)

2019 US clearance of OR30^o Dual Mobility with OXINIUM[◊] DH Technology

POLARCUP^{\lapha} demonstrates excellent clinical and functional outcomes





clinical publications



4





Excellent cumulative 10-year survivorship (all cause)¹¹ **95.9%** n=502





Dislocation rate in primary THR:¹¹⁻¹³ 0.0 to 0.7%



OXINIUM femoral head

Launched in 2002; currently used with POLAR3 and REDAPT Total Hip Solutions

- Ceramicised metal: oxidized zirconium is a metallic alloy

with a ceramic surface that

provides wear resistance without brittleness

- OXINIUM minimizes the risk of corrosion and fretting compared to CoCrMo¹⁴

- Biocompatibility: OXINIUM contains very low levels of nickel, cobalt and chromium compared to cobalt chromium molybdenum implants^{15,16}



Highly cross-linked polyethylene (XLPE) insert

Launched in 2002; currently used across entire Smith+Nephew hip platform

10 Mrad irradiated and remelted XLPE
Excellent mechanical properties¹⁷
No measurable free radicals¹⁷
Oxidation resistance¹⁸
Low wear rate with a marked reduction in the risk of revision for aseptic loosening¹⁹⁻²¹
Eccentric polyethylene design; reduces risk of impingement at retentive mouth



OXINIUM DH (Diffusion Hardened) liner

Launched in 2020
Diffusion hardened oxidized zirconium (OXINIUM) designed for hard-on-hard articulation²²
Comparable abrasion damage resistance to OXINIUM and superior to CoCrMo²³
Low wear rates under ideal and adverse conditions^{24,25}
18 degree taper and alignment peg designed to aid in liner insertion and seating²⁶



R3^{\phi} or REDAPT^{\phi} Acetabular Systems

Continuum of care from primary to complex revisions with acetabular platform
Modular shell designs enabling screw fixation
Liner removal slot

OR3O[◊] delivers...

Low wear rates

OR30 may deliver reduced XLPE wear rates compared to POLARCUP⁶ under idealised conditions (ORS1041) and under adverse subluxation (ORS1012)^{24,25}

Adequate clearance to accommodate deformation

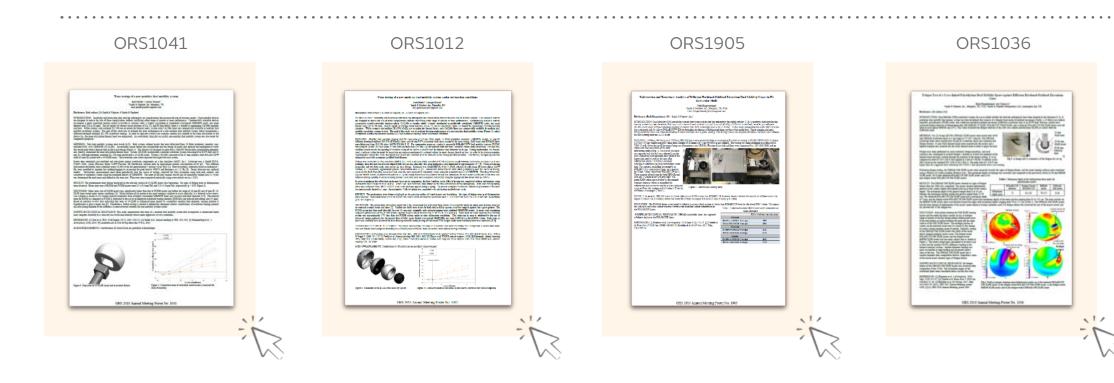
OR30 device has been shown to incorporate adequate clearance between the insert and liner to accommodate acetabular shell/liner deformation that may occur upon implantation; it should perform similarly to POLARCUP (ORS1905)²⁷

Minimal fatigue failure

OR30 insert will withstand stresses anticipated by sub-optimal acetabular cup orientation, and is comparable to POLARCUP (ORS1036)²⁸

Improved corrosion resistance

OR30 may deliver improved corrosion resistance compared to CoCrMo (ORS0528)²⁹

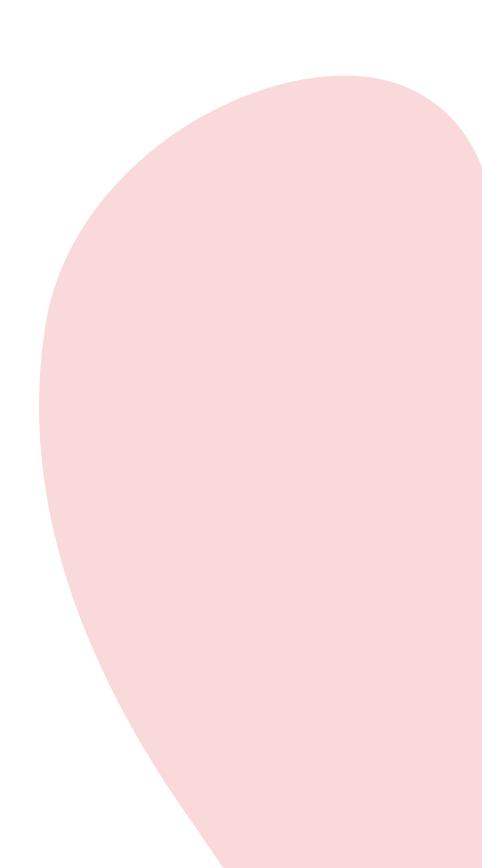


ORS0528	
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Indications for OR30^{\$*30}

- Advanced degeneration of the hip joint as a result of degenerative, post-traumatic, or rheumatoid arthritis
- Fracture or avascular necrosis of the femoral head
- Failure of previous hip surgery: joint reconstruction, internal fixation, arthrodesis, hemiarthroplasty, surface replacement arthroplasty, or total hip replacement
- All forms of osteoarthritis
- Patients with hips at risk of dislocation (incl. spinal deformity)
- Femoral neck fracture or proximal hip joint fracture

*This is a full list of the indications for OR3O; use of OR3O may not be suitable for all patients and should be decided by the surgeon on a per-patient basis.





OR30^{\$} Dual Mobility with

Stability redefined In black and white

Smith
 Nephew

OXINIUM^o DH Technology

References

1. Gwam CU, Mistry JB, Mohamed NS, et al. Current Epidemiology of Revision Total Hip Arthroplasty in the United States: Nation 2017:32:2088-2092. 2. Australian Orthopaedic Association National Joint Replacement Registry (AOANJRR) Hip, Knee & Shoulder Arthroplasty: 2019 com/annualreports-2019. Accessed April 30, 2020. 3. Moore C, Orlandini L. The dual mobility concept in total hip arthroplasty. Bone & Joint Science. 2012;4:1–4. 4. Blakeney WG, EpinetteJ-A, Vendittoli P-A. Dual mobility total hip arthroplasty: should everyone get one? EFORT Open Reviews. 5. Jones CW, De Martino I, D'Apolito R, Nocon AA, Sculco PK, Sculco TP. The use of dual-mobility bearings in patients at high risk A):41–5. 6. Abdel MP. Simplifying the hip-spine relationship for total hip arthroplasty: when do I use dual-mobility and why does it work? J 7. Epinette J-A, Lafuma A, Robert J, Doz M. Cost-effectiveness model comparing dual-mobility to fixed-bearing designs for total Traumatology: Surgery & Research. 2016;102:143-148. 8. De Martino I, Triantafyllopoulos GK, Sculco PK, Sculco TP. Dual mobility cups in total hip arthroplasty. World J Orthop. 2014;18; 9. Neri T, Philippot R, Klasan A, et al. Dual mobility acetabular cups for total hip arthroplasty: advantages and drawbacks. Expert 10. Orthopaedic Data Evaluation Panel (ODEP). Available at: <u>http://www.odep.org.uk</u>. Accessed March 27, 2020. 11. Cypres A, Figuet A, Girardin P, et al. Long-term outcomes of a dual-mobility cup and cementless triple-taper femoral stem co retrospective analysis. J Orthop Surg Res. 2019;14(1):376. 12. Bauchu P, Bonnard O, Cypres A, Fiquet A, Girardin P, Noyer D. The dual-mobility POLARCUP: first results from a multicenter st 13. Fiquet A, Noyer D. "Polarsystem" dual mobility hip prosthesis and "minimally invasive surgery" (MIS). Interactive Surgery. 2006 14. Cartner J, Aldinger P, Li C, Collins D. Characterization of femoral head taper corrosion features using a 22-year retrieval datab **15.** Hunter G, Dickinson J, Herb B, Graham R. Creation of oxidized zirconium orthopaedic implants. J ATSM Int. 2005;2:7. 16. ASTM F75-01. Standard specification for cobalt-28 chromium-6 molybdenum alloy castings and casting alloy for surgical imp Conshohocken, PA, 2012. 17. Morrison M, Jani S. Comparison of sequential and single-dose irradiation effects on the mechanical and physical properties of Research Society Congress; February 14–18, 2007; CA, USA.

al Inpatient Sample 2009 to 2013. J Arthroplasty.
Annual Report. Available at: <u>https://aoanjrr.sahmri.</u>
of dislocation. Bone Joint J. 2019;101-B(1 Supple
I Arthroplasty. 2019;34:S74–S75. hip replacement in France. Orthopaedics &
180–187. Rev Med Devices. 2018;15:835–845.
ombination in total hip replacement: a multicenter
tudy. Orthopedics. 2008;31(12 Suppl 2):97–99. 5;22:1–5. base. HSSJ. 2017;13:35–41.
plants (UNS R30075), ASTM International, West
UHMWPE. Poster 1786 presented at Orthopaedic
• • • • • • • • • • • • • • • • • • • •

References

18. Morrison ML, Jani S. Evaluation of sequentially crosslinked ultra-high molecular weight polyethylene. J Biomed Mater Res B Appl Biomater. 2009;90:87–100.
19. Davis ET, Pagkalos J, Kopjar B. Polyethylene manufacturing characteristics have a major effect on the risk of revision surgery in cementless and hybrid total hip arthroplasties:
an analysis of the National Joint Registry Of England, Wales, Northern Ireland and The Isle of Man. Bone Joint J. 2020;102-B(1):90–101.
 Jassim S, Patel S, Wardle N, et al. Five-year comparison of wear using oxidised zirconium and cobalt–chrome femoral heads in total hip arthroplasty. Bone Joint J. 2015;97:883– 889.
21. Parikh A, Hill P, Pawar V. The effect of femoral head diameter and material on the wear of highly crosslinked polyethylene liners. Abstract #042 Presented at Society for Biomaterials Annual Meeting; April 13–16, 2011; FL, USA.
22. Pawar V, Weaver C, Parikh A, Jani S. Evaluation of Diffusion Hardened Oxidized Zr-2.5wt%Nb for Hard-on-Hard Articulation in Total Hip Arthroplasty. Medical Device Materials VI; Proceedings from the Materials & Processes for Medical Devices Conference 2011 (ASM International). 2013;149–152.
23. Parikh A, Weaver C, Sprague J, Pawar V. Abrasion resistance, wear performance, and taper corrosion of a new composition of ceramicised metal. Poster 1910 presented at Orthopaedic Research Society Congress; March 5–8, 2016; FL, USA.
24. Parikh A, Weaver C. Wear testing of a new modular dual mobility system under subluxation conditions. Poster 1012 presented at Orthopaedic Research Society Congress; February 2–5, 2019; TX, USA.
25. Parikh A, Weaver C. Wear Testing of a New Modular Dual Mobility System. Poster 1041 presented at ORS Congress; February 2–5, 2019; TX, USA.
26. Lee Y-K, Kim K-C, Jo W-L, Ha Y-C, Parvizi J, Koo K-H. Effect of inner taper angle of acetabular metal shell on the malseating and dissociation force of ceramic liner. J Arthroplasty. 2017;32:P1360–1362.
27. Bingenheimer H. Deformation and roundness analysis of diffusion hardened oxidized zirconium dual mobility liners in r3 acetabular shells. Poster 1905 presented at Orthopaedic Research Society Congress; February 2–5, 2019; TX, USA.
28. Bingenheimer H, Li C. Fatigue test of a cross-linked polyethylene dual mobility insert against diffusion hardened oxidized zirconium liner. Poster 1056 presented at Orthopaedic Research Society Congress; February 2–5, 2019; TX, USA.
29. US Department of Health and Human Services. 510(k) Summary Smith & Nephew OR3O Dual Mobility System (K191002). Available at: https://www.accessdata.fda.gov/cdrh_docs/pdf19/K191002). Available at: https://www.accessdata.fda.gov/cdrh_docs/pdf19/K191002). Available at: https://www.accessdata.fd

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2020 Smith & Nephew
24756-en V2 12/20.
Published December 2020.

