

Design Rationale



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Rediscover normal

Introduction

While literature reports good outcomes for many current knee systems, clinical scores do not necessarily reflect patient satisfaction. While this dissatisfaction could be attributed to abnormal motion, such as paradoxical motion and AP instability, doday's active patients simply expect more out of their knee replacements than ever before. These expectations are not being met by the current generation of knee replacement designs.

In an effort to replicate normal knee function, Smith & Nephew conducted in-depth analyses of the geometry, kinetics, kinematics and ligament behavior of the normal knee and conventional TKA systems. These analyses created a better understanding of how the normal knee works and the limitations inherent in current knee designs. The knowledge gained through this research fueled the creation of a knee system to address those limitations.

The JOURNEY° Bi-Cruciate Stabilised Knee System was shown to replicate both the PCL and ACL function, promote recovery of normal muscle activity, accommodate deep flexion, induce normal tibiofemoral axial rotation and provide proper patellar tracking throughout the entire range of flexion.⁵⁻¹⁹ Building upon that history, the JOURNEY II Total Knee System has refined the design and expanded the system to include cruciate retaining, deep dished, and constrained posterior stabilised options.

JOURNEY II knees were designed to achieve normal shapes, position and motion. Smith & Nephew created this platform to empower patients to rediscover normal post total knee arthroplasty.

Indications

Indications for use include rheumatoid arthritis; post-traumatic arthritis, osteoarthritis or degenerative arthritis; failed osteotomies or unicompartmental replacement.* This system is designed for use in patients in primary total knee replacement surgery. Posterior stabilised knee systems are designed for use in patients where the anterior and posterior cruciate ligaments are incompetent and the collateral ligaments remain intact. Constrained knee systems are designed for use in patients where the posterior cruciate ligament and one or both of the collateral ligaments (i.e. medial collateral and/or lateral collateral ligament) are incompetent.

Achieving normal kinematics

The guiding principle behind the design of the JOURNEY° II Total Knee System was to achieve near normal function and motion while maintaining excellent durability and having the robustness to accommodate surgical and patient variability.

How to achieve normal

Shapes. Position. Motion.

To restore the native 3° Varus joint-line, the medial condyle on the JOURNEY II Femoral component was designed to be thicker both distally and posteriorly than the lateral condyle. This unique design was created to restore the knee's native morphological surfaces while allowing the surgeon to make cuts perpendicular to the mechanical axis. Like the human knee, the posterior condyles in the JOURNEY II femoral component have been designed to be circular in shape; allowing for soft tissue influence in axial rotation and overall physiological performance.

The medial and lateral articular surfaces designed into the polyethylene insert allow the surgeon to restore proper knee kinematics:

Medial – Concave shape promotes pivot Lateral – Convex shape promotes rollback

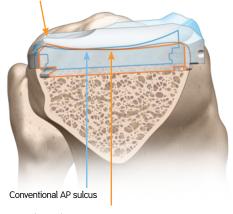
The insert sulcus design replicates the AP midline found in the human knee, allowing restoration of tibio-femoral articulations without paradoxical motion. To accommodate deep flexion, the convex lateral surface in the sagittal plane creates a slight posterior slope. ^{8, 9, 12, 35, 41}

Durability/Robustness

- Wear VERILAST° Technology combines OXINIUM° and XLPE to form a highly durable and long-lasting bearing combination.²⁵⁻³³
- OXINIUM Oxidised Zirconium, exclusively from Smith & Nephew, contains <0.0035% nickel content compared to 0.5% in cobalt chrome.
- Surgical robustness All the benefits of improved function and motion with similar sensitivity to surgical and patient variability as conventional knee systems.³⁴

Medial

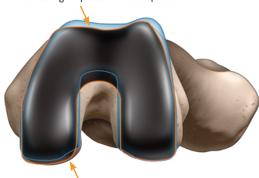
Prominent posterior medial lip provides stability and promotes normal kinematics^{5, 9, 13, 35, 41}



Normal AP sulcus position prevents paradoxical motion 9,12,35,41

Femur

Anatomic, asymmetric flange is designed to prevent overstuffing the patellofemoral compartment



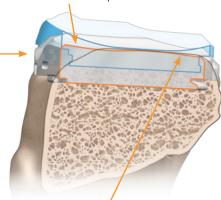
Restores anatomic 3° distal and posterior femoral joint line providing more normal ligament strain and patello-femoral tracking ^{22, 24, 35, 41}

Lateral

JOURNEY II TKA

Conventional TKA

Smaller anterior lateral lip allows screw home⁹



Normal convexity provides increased posterior lateral slope to facilitate anatomic lateral femoral rollback and external rotation ^{5, 9, 35, 41}

Advanced design tools and methods

Sizing and fit

To design the JOURNEY° II Total Knee System, statistical data from over 250 femurs and tibias was used to characterise articular shapes and resected profiles in an effort to optimise four types of fit:

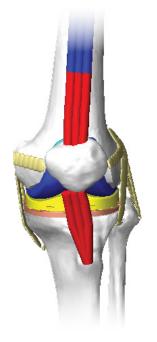
- Coverage fit coverage of resected bone
- Resection fit resection required to attach implants to bone
- Interface fit implant/bone interface stability
- Biomechanic fit restoration of functional surfaces
- This wealth of data showed clear dimensional and size differences across a variety of unique patient anatomy that required a non-linear progression of more anatomic and personalised implant dimensions throughout the size range as seen below:
- Bone coverage was optimised by providing asymmetric baseplates and 10 (non-scaled) femoral sizes⁴²
- Bone resections were minimised by angling the PS box and posterior resection for all sizes⁴³
- Through a unique femoral 'hooking' implantation method that helps pressurise the cement and lock the implant to the femur⁴⁵
- Biomechanic fit was improved by restoring the sagittal profiles, trochlear depth and jointline^{22, 24, 35, 41}

The result is a system that is anthropometrically optimised.44

Fluoroscopy Medial

Top

Frontal

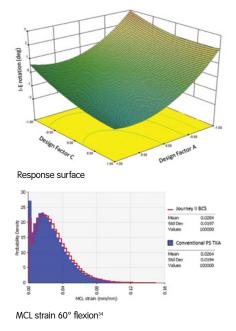


Characterise → Optimise → Analyse

The JOURNEY II Total Knee System was designed using state-of-the-art computer simulation and optimisation techniques. Parametrically controlled CAD models were virtually implanted in an advanced computer knee simulator (proprietary, enhanced version of LifeMOD™/KneeSIM™) and analysed during multiple activities including deep knee bend and gait.

Key measures including kinematics and ligament strain, which have been correlated to in vivo⁵ and in vitro data²⁰ respectively, were collected throughout flexion to characterise the biomechanic performance of the design. This allowed targeted advancements over previous total knee designs including JOURNEY BCS to further close the gap between total knee arthroplasty and normal healthy knees.⁴¹ Output from LifeMOD/KneeSIM was processed using the following:

- Characterise: Design of Experiments to characterise implant behavior and identify the most influential design parameters
- Optimise: Response Surface Methodology to optimise the implant shapes
- Analyse: Monte Carlo Simulations to evaluate surgical sensitivity on multiple patients compared to conventional knee designs
- During development of the JOURNEY II Total Knee System, hundreds of thousands of combinations³⁴ of implant designs, patient anatomy, and surgical positioning were simulated, which is impossible to accomplish using conventional implant design methods. The resulting optimised design maintains the anatomic shapes of the original JOURNEY BCS design and uses subtle enhancements to expand the benefits of normal shapes, position and kinematic motion.⁴⁶



Normal knee function

Shape

Joint line

- Medial condyle more distal than lateral condyle
- 3° physiological joint line

Femur

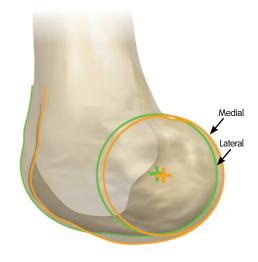
- Distal lateral condyle less round than the medial condyle
- · Lateral posterior offset less than medial
- · Posterior condyles circular in shape

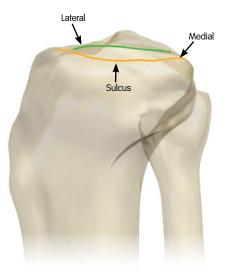
Tibia

- Medial concave surface
- Medial sulcus near AP midline
- · Lateral convex surface

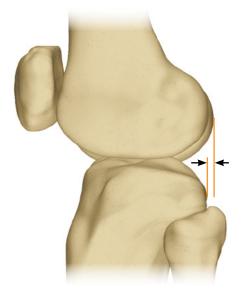
AP stability

- ACL provides anterior stability and limits anterior translation of the tibia (femoral posterior translation)
- PCL provides posterior stability and limits posterior translation of the tibia (femoral anterior translation)
- Medial sulcus causes the medial posterior femoral condyle to sit nearly flush with the posterior tibia
- In this anterior position, the force environment causes femoral rollback during flexion





Concave medial, convex lateral surface



Anterior AP position

Kinematics and ligament behavior 21, 22

Extension

0° - Screw-home, anterior AP position

- Tibial tubercle approximately 10mm lateral to the ML midline
- Femur internally rotated 5° "screw-home" creating a Q-angle of 14-17°
- Sulcus of medial side and ACL cause the femur to sit nearly flush with the posterior tibia

Mid-flexion

0 - 90° - Rollback medial pivot

- Because of the anterior position of the femur, forces during flexion direct the femur to roll back
- During flexion, the quadriceps mechanism attempts to straighten and applies external rotation torque to the femur through the patella
- Femur external axial rotation is aided by the downhill force of the convex lateral compartment
- Axial rotation occurs due to greater lateral than medial rollback until the quadriceps mechanism is straight and the Q-angle is minimised
- Rollback combined with femoral external axial rotation yields a medial pivot
- MCL strain is near constant 0-60° before starting to slacken
- LCL strain gradually decreases with flexion
- PCL strain increases with flexion aiding femoral rollback

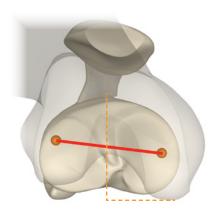
Deep-flexion

90 - 155° - Posterior translation

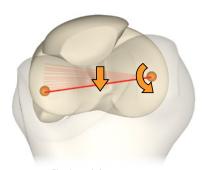
- Femur translates further posteriorly
- Femoral axial rotation continues due to lateral rollback while medial rollback has small changes and may decrease
- · MCL continues to become looser with flexion
- PCL strain reaches its peak without becoming overly tight and limiting flexion

Functional flexion

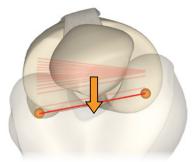
- Lateral posterior offset is less, so femoral external axial rotation and convex lateral compartment are necessary for lateral condyle to clear tibia
- Medial condyle is more anterior than the lateral condyle, therefore, large posterior offset is needed to clear tibia
- Femoral external axial rotation and lateralised patella groove minimises patellofemoral ML shear force, which optimises quadriceps mechanism function



 0° – Screw-home, anterior AP position



0-90° – Rollback medial pivot



90-155° – Posterior translation

Conventional TKA function

Shape

Joint line

- · Medial and lateral condyles equal thickness
- Non-physiological 0° joint line

Femur

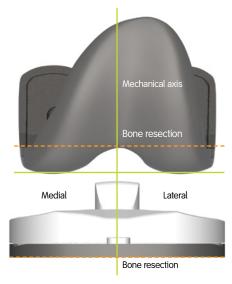
- · Symmetric distal condyles identical in thickness and shape
- Symmetric posterior condyles identical in thickness and shape

Tibia

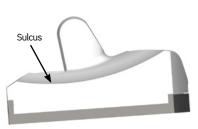
- Symmetric insert identical in thickness and shape, creating a bi-concave design
- Sulcus located in posterior 1/3 of insert
- Symmetric baseplate does not provide anatomic coverage

AP stability

- Lack of ACL replicating feature causes anterior instability, especially in early gait while small tibial insert posterior lips further limits anterior stability
- Posterior cam or PCL provides posterior stability and limits anterior translation of the femoral component
- Insert sulcus causes the posterior femoral condyles to overhang the tibia posteriorly
- In this posterior position, the force environment causes femoral paradoxical anterior translation during flexion



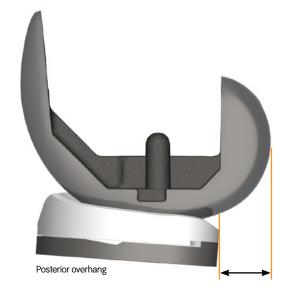
0° non-physiological joint line



Concave medial



Concave lateral



Kinematics and ligament behavior

Extension

0° - No screw-home, posterior overhang

- Symmetric insert causes femoral component/femur to be directed anteriorly
- This results in no screw-home, reducing Q-angle
- Posterior sulcus and lack of an ACL cause the femur to overhang the tibia posteriorly
- This may require continuous use of the quadriceps muscle to stand, causing fatigue

Mid-flexion

0° - 90° - Paradoxical motion, lateral pivot

- Because of the posterior position of the femoral component, forces during flexion direct the femur to paradoxically translate anteriorly
- During flexion, the quadriceps mechanism attempts to straighten and applies external rotation torque to the femur through the patella
- Femoral external axial rotation resisted by insert bi-concave conformity
- Q-angle is not minimised, causing patellofemoral ML shear force
- Paradoxical anterior translation combined with limited femoral external axial rotation yields a lateral pivot
- MCL strain remains near constant 0-90° which could result in more tension than normal in some conventional designs. In others the MCL becomes slack in mid-flexion before regaining tension by 90°, which could contribute to mid-flexion instability.
- LCL strain is likely looser than normal in extension because femur sits more posterior.
- When the PCL is retained, its strain increases with flexion aiding femoral rollback, but it is likely looser than normal in extension because the femur sits more posterior, which could reduce early flexion stability

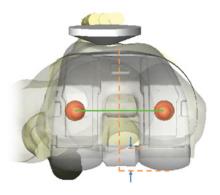
Deep-flexion

90° - Max flexion - Posterior translation, abnormal rotation

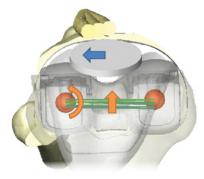
- Posterior cam causes femoral posterior translation
- Insert bi-concave conformity exceeds external torque applied by the quadriceps mechanism
- Femoral component abnormally rotates internally and aligns with symmetric insert
- Posterior translation combined with femoral abnormal internal rotation yields a lateral pivot
- Q-angle is increased, causing significant patellofemoral ML shear force
- MCL strain continues to remain constant which could restrict flexion
- When the PCL is retained, its strain reaches its peak but is often tighter than the normal knee²³ which could inhibit high flexion

Functional flexion

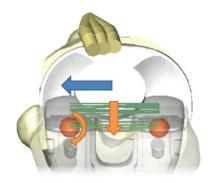
- Lateral posterior offset is less, so femoral internal axial rotation and concave lip of lateral insert may cause early bone impingement, limiting flexion
- Large patellofemoral ML shear force may cause anterior knee pain, which can limit functional flexion



 0° – No screw-home, posterior overhang



0-90° – Paradoxical motion, lateral pivot



>90° - Posterior translation, abnormal axial rotation

JOURNEY® II Total Knee System function

Shape

Joint line

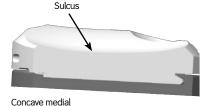
- Medial condyle more distal than lateral condyle
- 3° physiological joint line created

Femur

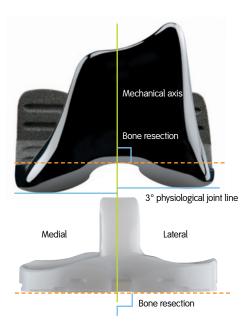
- Lateral distal condyle less thick than medial femoral condyle
- Asymmetric posterior offset of medial and lateral condyles maintained
- · Posterior condyles circular in shape

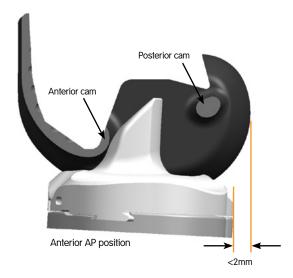
Tibia

- Concave medial surface
- Medial sulcus near AP midline
- Lateral compartment thicker than the medial compartment
- Convex lateral surface in sagittal plane creates a slight posterior slope

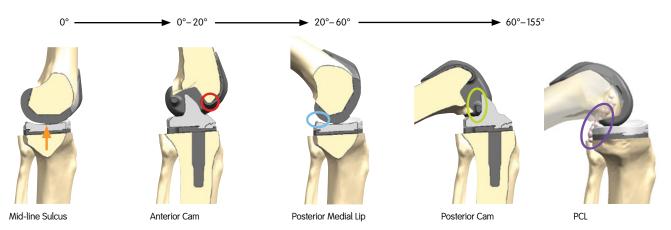








Stability throughout a range of motion



Kinematics and ligament behavior

Extension

0° - Screw-home, anterior AP position

- Insert arcuate path allows for 5° of screw-home
- Sulcus of medial side causes the femur to sit nearly flush with the posterior tibia
- · Normal Q-angle and AP position created in extension

Mid-flexion

0° - 90° - Rollback medial pivot

- Because of the anterior position of the femur, forces during flexion direct the femur to roll back
- During flexion, the quadriceps mechanism attempts to straighten and applies external rotation torque to the femur through the patella
- Femur external axial rotation is aided by the downhill force of the convex lateral compartment
- Rotation continues until the quadriceps mechanism is straight and the Q-angle is minimised
- Rollback combined with femoral external axial rotation yields a medial pivot
- MCL strain is near constant 0-60° before starting to slacken
- · LCL strain gradually decreases with flexion
- When the PCL is retained, its strain increases with flexion aiding femoral rollback plus the PCL is under some tension in extension due to the anatomic anterior position of the femur, which provides early flexion stability

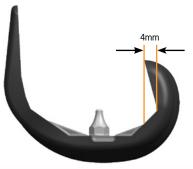
Deep-flexion

90° - 155° - Posterior translation

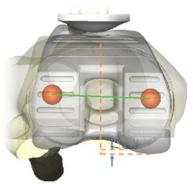
- Femur translates posteriorly
- MCL continues to become looser with flexion which allows for high flexion
- When the PCL is retained, its strain reaches its peak but less tight than conventional knees, which allows for high flexion

Functional flexion

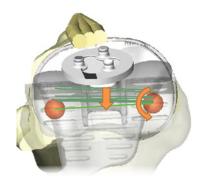
- 15° flexed cut extends articular surfaces by 4mm while minimising bone resection
- Lateral posterior offset is less, so femoral external axial rotation and convex lateral compartment are necessary for lateral condyle to clear tibia
- Medial condyle is more anterior than the lateral condyle, therefore, large posterior offset is needed to clear tibia
- Femoral external axial rotation and lateralised patella groove from anatomic asymmetric femoral condyles designed to minimise patellofemoral ML shear force and maintain normal quadriceps mechanism function¹⁴



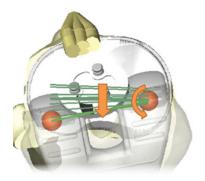
15° flexed cut extends the articular surfaces



0° - Screw-home, anterior AP position

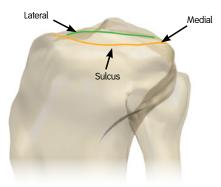


0° – 90° – Rollback medial pivot



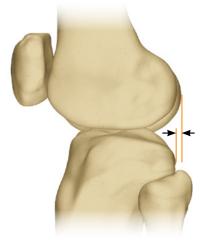
90° – 155° – Posterior translation

Function summary





- Concave medial surface
- Sulcus near AP midline
- · Convex lateral surface
- 3° physiological joint line



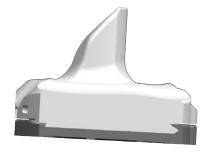
AP stability - Normal knee

- · ACL provides anterior stability
- PCL provides posterior stability
- Anterior AP position causes femoral rollback



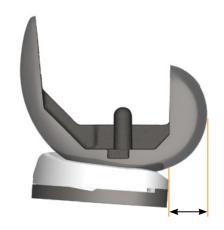
Shape - Conventional TKA

- Symmetric concave medial and lateral surfaces
- Sulcus located in posterior 1/3
- 0° unnatural joint line



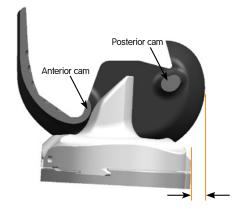
Shape - JOURNEY® II Total Knee System

- Concave medial surface
- Sulcus near AP midline
- Convex lateral surface
- 3° physiological joint line



AP stability - Conventional TKA

- Lack of anterior stability (ACL function)
- Posterior overhang causes femoral paradoxical anterior translation
- Anterior and mid-flexion instability

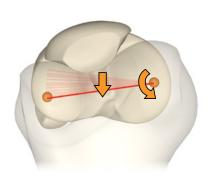


AP stability – JOURNEY II Total Knee System

- Anterior cam and posterior medial lip provide anterior stability
- Anterior AP position causes femoral rollback
- ACL function and femoral rollback provide anterior and mid-flexion stability

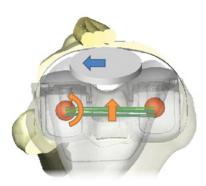
Conventional TKA function

AP stability	Ant. instak (No ACL function	,	Mid-flex (Paradoxica			/			(Posterio Over ter Posterior ca	ision o	r reduc		bility	
Kinematics	No screw-home		al pivot exical motion	and limit	ted axial r	otation)			Posterio Posterior ca		lation			
Flexion	Adequate	quadr	iceps eff	iciency	/	Р	atellofe	emora	l ML :	shear s	tresses	s increa	ase		
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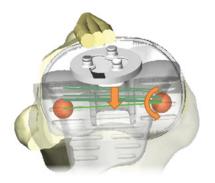
Kinematics - Normal knee

- 0° Screw-home, anterior AP position
- 0° 90° Rollback plus femoral external axial rotation yields medial pivot
- 90° 155° Posterior femoral translation



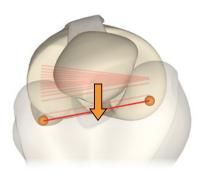
Kinematics - Conventional TKA

- 0° No screw-home, posterior overhang
- 0° 90° Paradoxical motion plus limited axial rotation yields lateral pivot
- 90° 155° Abnormal femoral internal axial rotation



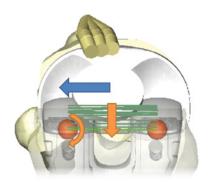
Kinematics – JOURNEY° II Total Knee System

- 0° Screw-home, anterior AP position
- 0° 90° Rollback plus femoral external axial rotation yields medial pivot
- 90° 155° Posterior femoral translation



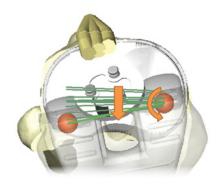
Flexion - Normal knee

- External axial rotation of femur allows lateral condyle to clear posterior tibia
- Large posterior offset allows medial condyle to clear posterior tibia
- Patellofemoral ML shear force minimised



Flexion - Conventional TKA

- Abnormal internal axial rotation causes early bone impingement, limiting flexion
- Internal axial rotation and centralised distal patella track causes significant patellofemoral ML shear force



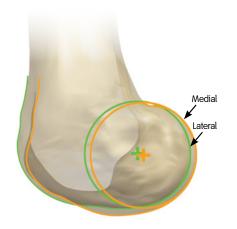
Flexion - JOURNEY II Total Knee System

- External axial rotation of femur allows lateral condyle to clear posterior tibia
- Large posterior offset allows medial condyle to clear posterior tibia
- Patella is designed to minimise shear force by tracking laterally similar to the normal knee³⁵

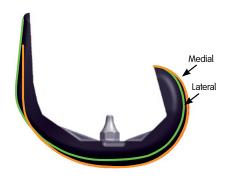
JOURNEY II Total Knee System function

AP stability	Ant. stak (Anterior car	,								•						
Kinematics	Screw-home	Screw-home Medial pivot (Convex lateral and concave medial)								Posteri Asymmet						
Flexion	Enhance	d qua	driceps	effici	ency					Ninimize xtended				hear st	ress	
	-5 0 1	0 2	0 30	40	50	60	, ,	80 lexion	90	100	110	120	130	140	150	155

Ligament behavior







Ligament behavior - Normal knee

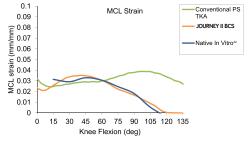
- Asymmetric femoral condyles affect tension profile of medial and lateral soft tissues differently
- MCL strain is near constant 0-60° before starting to slacken²²
- LCL strain gradually decreases with flexion²²
- PCL strain increases with flexion up to its peak in deep flexion without being overly tight

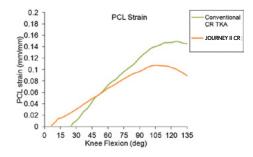
Ligament behavior - Conventional TKA

- Symmetric femoral condyles can not replicate normal tension profile of medial and lateral soft tissues without femoral malalignment
- MCL strain is typically near constant throughout flexion which could restrict deep flexion or loose in mid-flexion which could cause instability
- LCL strain is likely looser than normal in extension because femoral sits posterior
- PCL strain is looser in extension which could affect knee stability and tighter in deep flexion which could restrict deep flexion

Ligament behavior – JOURNEY° II Total Knee System

- Asymmetric femoral condyles allow replication of normal tension profiles of both medial and lateral soft tissues^{22,41}
- MCL strain is near constant 0-60° before starting to slacken
- LCL strain gradually decreases with flexion
- PCL strain increases with flexion up to its peak in deep flexion without being overly tight





Ligament behavior comparison - MCL strain⁴¹

Ligament behavior comparison - LCL strain⁴¹

Ligament behavior comparison - PCL strain 35

Durability

Conventional TKA wear

- Paradoxical motion during flexion may increase sliding distance/wear⁴⁰
- Concave lateral insert conformity increases the wear footprint (the total amount of area that the femoral traverses during the entire ROM), which may increase wear

Conventional TKA post contact

- Unintended femoral contact with the post causes severe post stresses
- Surpassing fatigue stress can cause post breakage
- Non-rounded posts and cams can cause edge loading during femoral external axial rotation, increasing stresses on the post

Conventional TKA patellofemoral shear forces

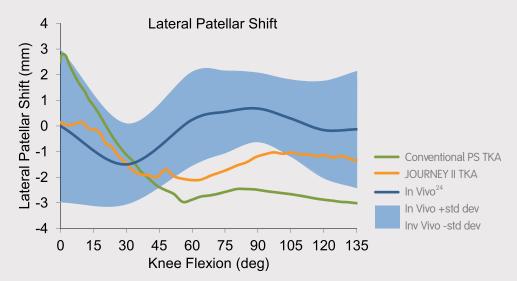
- Limited and abnormal femoral axial rotation increases patellofemoral ML shear forces
- Excessive shear force may cause anterior knee pain, premature articular wear and/or peg breakage

Conventional TKA materials

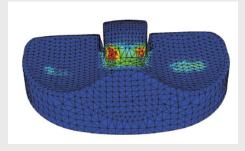
- CoCr is less abrasion resistant and is less lubricious than OXINIUM° Oxidised Zirconium, increasing both adhesive and abrasive wear^{36,37,38}
- Non-polished baseplates produce more backside wear than polished baseplates

Conventional TKA locking mechanism

 Competitive insert/baseplate locking mechanisms require a screw or bolt augment through the insert to prevent insert disassociation



Patella tracking comparison 35



Conventional PS post edge impingement



Wear simulator



JOURNEY° II TKA

Durability (continued)

JOURNEY° II TKA wear

- Wear tested to five million cycles³²
- Predominant wear feature on the insert articular surface was burnishing³²
- There were no signs of fatigue wear or delamination³²
- Volumetric wear was less than previously published wear for conventional TKA²⁵⁻³³
- Medial pivot and rollback cause the lateral side to roll more and slide less and virtual elimination of paradoxical sliding as the knee flexes should maintain the normal cycles of the femur across the polyethylene leading to reduced wear compared to conventional designs⁴⁴
- Convex lateral insert compartment reduces wear footprint⁴⁴

JOURNEY II BCS Knee System post contact

- Large, rounded anterior cam reduces contact stresses and eliminates edge loading^{48, 49}
- Asymmetric, rounded posterior cam maintains congruent contact during femoral axial rotation, eliminating edge loading and minimising stress⁵⁰

JOURNEY II TKA patellofemoral ML shear forces

 Femoral external axial rotation and patella groove lateralised by asymmetric femoral condyles are designed to reduce patellofemoral ML shear forces, risk of premature wear, peg breakage and anterior knee pain

JOURNEY II TKA materials

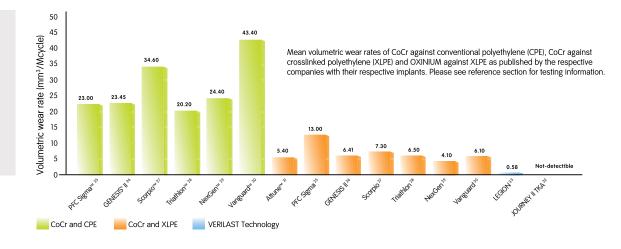
- OXINIUM^o Oxidised Zirconium reduces abrasive and adhesive wear²⁶
- Highly cross-linked polyethylene (XLPE) combines with OXINIUM to form VERILAST Technology a highly durable bearing combination shown have low wear rates during simulator testing²⁶
- ETO sterilisation does not produce free radicals, which reduces the risk of oxidation and subsequent delamination³⁹
- Polished tibial baseplate reduces backside wear⁴⁷

JOURNEY II TKA locking mechanism

- Strategic interference designed to reduce micromotion
- · Insertion tool provides confidence of proper assembly
- Large dovetail interface area eliminates the need for additional locking mechanisms (i.e. screws, clips)
- Deep flexion possible



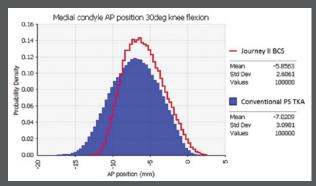
The implants identified to the right were tested by their manufacturers using different testing protocols and, therefore, the results are not directly comparable.



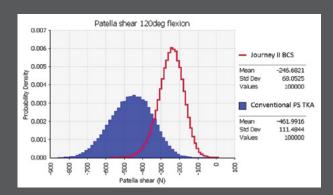
Robustness

Surgical sensitivity analysis

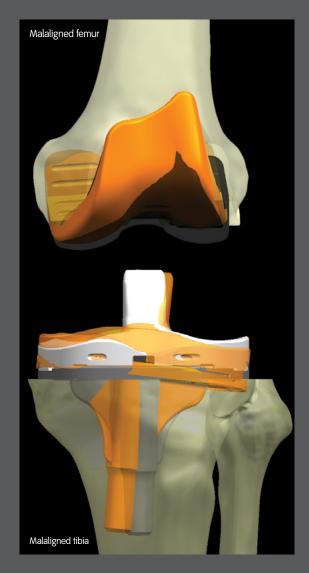
- Used to determine how sensitive JOURNEY® II Total Knee System is when not implanted in optimal alignment
- Response Surface Methodology was used to create a model of the effects of deviations from ideal surgical alignment
- Distributions, based on literature, were assigned to the surgical deviations. Then, Monte Carlo Analysis simulated a patient performing a deep knee bend after 100,000 random surgeries to identify the effects on knee joint loads, ligament strain, and kinematics for JOURNEY II and compared them to conventional TKA
- The distribution of outcomes from the surgical sensitivity analysis³⁴ showed JOURNEY II system has:
- · Lower worst case patella shear
- Similar or lower likelihood of overly tight ligaments
- More normal kinematics even when malaligned than a conventional TKA design



Variation in kinematics due to surgical variation³⁴



Variation in patella shear due to surgical variation. Left, more negative number, is higher shear force³⁴

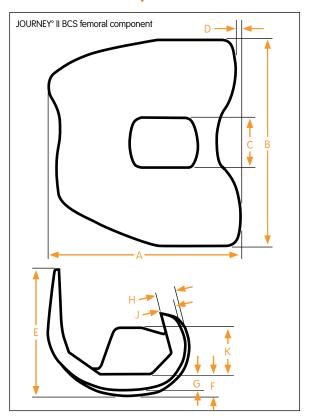


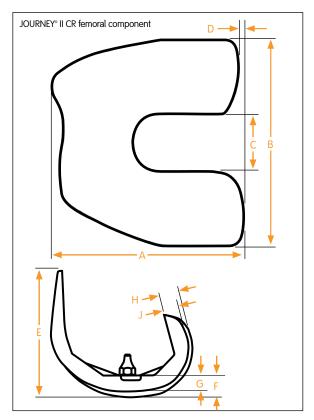
Surgical Variable	Max. Value	Min. Value
Femoral Joint Line	Superior4mm	Inferior 2mm
Femoral Anterior-Posterior	Anterior 2mm	Posterior 2mm
Femoral Varus-Valgus	Valgus4°	Varus 4°
Femoral Internal-External	External 6°	Internal 6°
Tibial Posterior Slope	Posterior 9°	Anterior 3°
Tibia Internal-External	External 6°	Internal 6°
Tibia Varus-Valgus	Varus 6°	Valgus 6°
Extension Gap	4mm gap	2mm interference

Surgical sensitivity

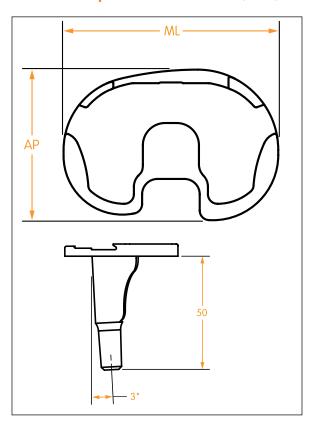
System overview

Femoral component dimensions (mm)





Tibial baseplate dimensions (mm)

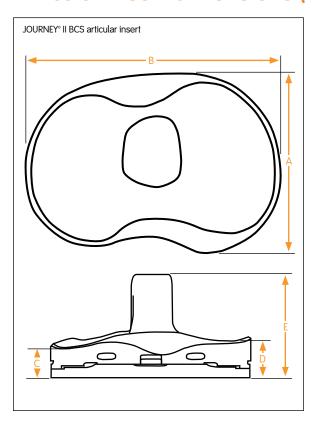


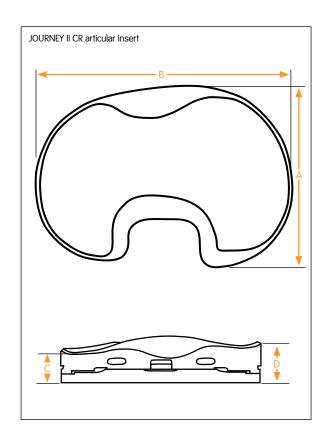
						Offset		VC	55 V	essidur
	AnteriorP	osterior Medial.	ateral Add	Width	targe H	offed Distal	nedial.	hick	es di Tricko	es hidre jid Trida jid Tri
	Arterio:	Medial.	88 C4	Poste	trauge,	Distal	Oiets	40g	Poster	BOT HEV
Size	Α	В	С	D	E	F	G	Н	J	K
1	51.7	59.0	16.5 / 19	1.7	49.5	9.5	7	9	7.4	16.0
2	53.7	60.0	16.5 / 19	1.7	50.7	9.5	7	9	7.4	17.0
3	56.7	61.5	16.5 / 19	1.7	52.5	9.5	7	9	7.4	17.0
4	59.7	64.5	16.5 / 19	1.7	54.3	9.5	7	9	7.4	20.5
5	62.7	67.5	16.5 / 19	1.7	56.0	9.5	7	9	7.4	20.5
6	65.7	70.5	16.5 / 19	1.8	57.7	9.5	7	9	7.4	22.0
7	68.8	73.5	16.5 / 19	1.8	59.5	9.5	7	9	7.4	22.0
8	71.8	76.0	16.5 / 19	1.8	61.2	9.5	7	9	7.4	22.0
9	75.8	80.0	16.5 / 19	1.8	63.5	11.5	9	11	9.4	22.8
10	79.8	82.0	16.5 / 19	1.8	65.7	11.5	9	11	9.4	22.8

	od	sterio ¹ ate
	Anterior Po	Nedial de
Size	AP	ML
1	42	60
2	45	64
3	48	68
4	50	71
5	52	74
6	54	77
7	56	81
8	59	85
9	61	89

Note: Stem sloped 3° posteriorly. Stem length is 50mm on all nonporous sizes.

Articular insert dimensions (mm)





	Anterior Anterior	Medial	Medial*	derd* laterd	Post Miles
9mm BCS Insert	Α	В	С	D	E
Size 1-2	42	60	9.6	11.9	34.1
Size 3-4	48	68	9.6	11.6	35.1
Size 5-6	52	74	9.6	11.9	38.6
Size 7-8	56	81	9.6	11.9	40.1

Minimum polyethylene thickness for a 9mm metal-backed component is 6.7 mm on the medial side.

	Arterior Posterior	Wedial	Medial*	s lateral* lateral
9mm CR Insert	Α	В	С	D
Size 1-2	42	60	9.6	11.6
Size 3-4	48	68	9.6	11.6
Size 5-6	52	74	9.6	11.6
Size 7-8	56	81	9.6	11.6

Minimum polyethylene thickness for a 9mm metal-backed component is 6.7mm on the medial side.

Insert offering / compatibility (BCS, Constrained, Deep Dished)

	Fem	Femoral Size								
Insert Size	1	2	3	4	5	6	7	8	9	10
1-2		•	•	•						
3-4		•	•	•		•				
5-6				•	•	•	•	•	•	
7-8						•	•	•	•	•

JOURNEY II CR insert compatibility

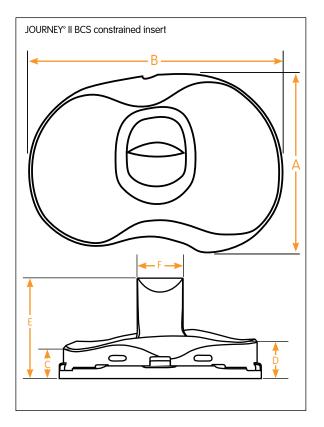
Completely interchangeable with all size femoral components

^{*}Baseplate thickness included.

^{*}Baseplate thickness included.

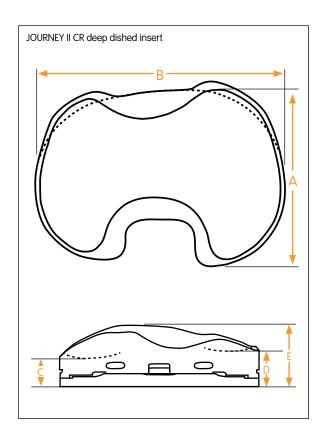
System overview (continued)

Tibial insert dimensions (mm)



	Arterio posterio	Medial ateral	Nedial Tricks	aleral chicks	post Heid	nt Post Width
9mm Constrained Insert	A	В	С	D	E	F
Size 1-2	42	60	9.6	12.1	34.1	16.1
Size 3-4	48	68	9.6	12.1	35.3	16.1
Size 5-6	52	74	9.6	12.1	38.6	16.1
Size 7-8	56	81	9.6	12.1	40.1	16.1

Minimum polyethylene thickness for a 9mm metal-backed component is 6.7 mm on the medial side.



	Anterior posterior	Medial eral	nedial thickness	s lateral rickne	ss Anterior Chickres
9mm Deep Dished Insert	Α	В	С	D	E
Size 1-2	42	60	9.6	12.1	16.9
Size 3-4	48	68	9.6	12.1	18.1
Size 5-6	52	74	9.6	12.1	19.3
Size 7-8	56	81	9.6	12.1	19.9

Minimum polyethylene thickness for a 9mm metal-backed component is 6.7mm on the medial side.

Insert offering / compatibility (BCS, Constrained, Deep Dished)

	Fem	noral	Size	•						
Insert Size	1	2	3	4	5	6	7	8	9	10
1-2		•	•							
3-4		•	•	•	•	•				
5-6				•	•		•			
7-8								•	•	

^{*}Baseplate thickness included.

^{*}Baseplate thickness included.

Summary

The JOURNEY® II Total Knee System is the next step for a knee system designed to restore normal function in that it maintains the tenets of restoring normal knee AP stability, kinematics and deep flexion while adding a Cruciate Retaining version, more stable Constrained PS and Deep Dished options, and enhancing the Bi-Cruciate Stabilised design. Smith & Nephew has continually improved the technologies used to better understand the behavior

of the knee from the kinematics to the soft tissue function to further advance the science behind knee arthroplasty design. With a design based on natural anatomy, the JOURNEY II Total Knee System addresses many of the problems associated with conventional systems, while maximising durability and minimising sensitivity to malpositioning.



function, motion and durability without sacrificing robustness required to work in the real world.



Notes	



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